

14

3150

REGULATORS

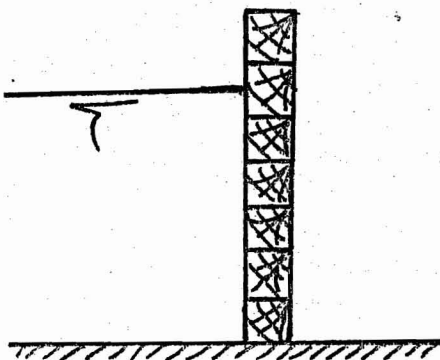
**DESIGN OF
SLIDING GATE**

Structure Design

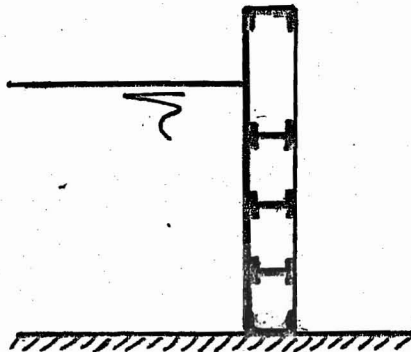
- 1- Design of Gate.
 - 2- Design of Gate Lifting Structure.
 - 3- Design of Pier.
 - 4- Design of Floor.
 - 5- Design of abutment and wing wall.
 - 6- Design of bridge.
-

1-Gates

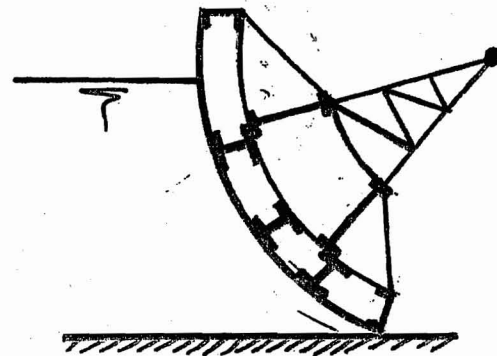
↓
Timber Gate



↓
Vertical Steel
Sliding Gate



↓
Radial Gate

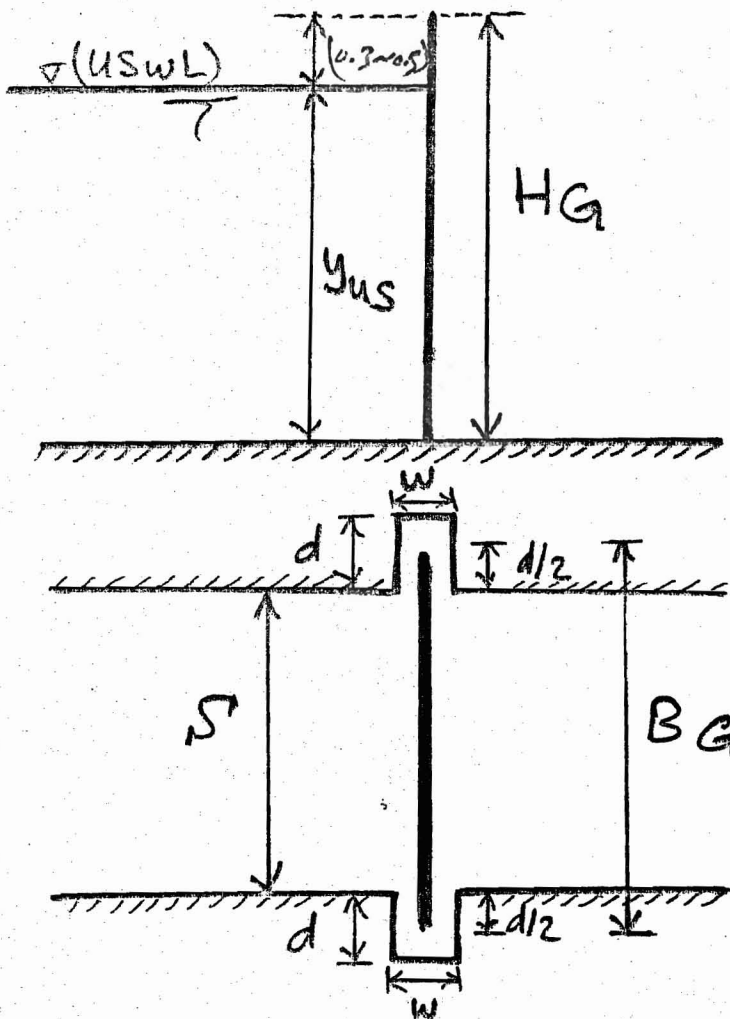


Sliding Gate

اول فطوره جب ژنه نده دل پيوابه Single gate و double gate

- If $S * y_{ds} < 16 \text{ m}^2 \rightarrow \therefore \text{use single gate}$
- If $S * y_{ds} \geq 16 \text{ m}^2 \rightarrow \therefore \text{use double gate}$

* Dimensions of single gate :-



$$H_G = y_{us} + (0.3 \rightarrow 0.5 \text{ m})$$

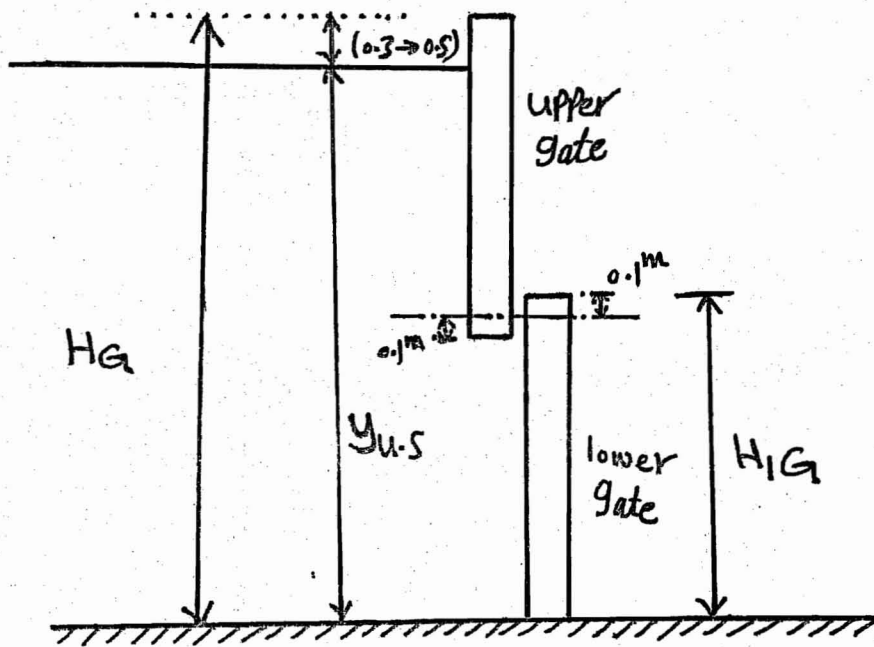
$$B_G = S + d$$

$$d = \frac{w}{3}$$

پيو

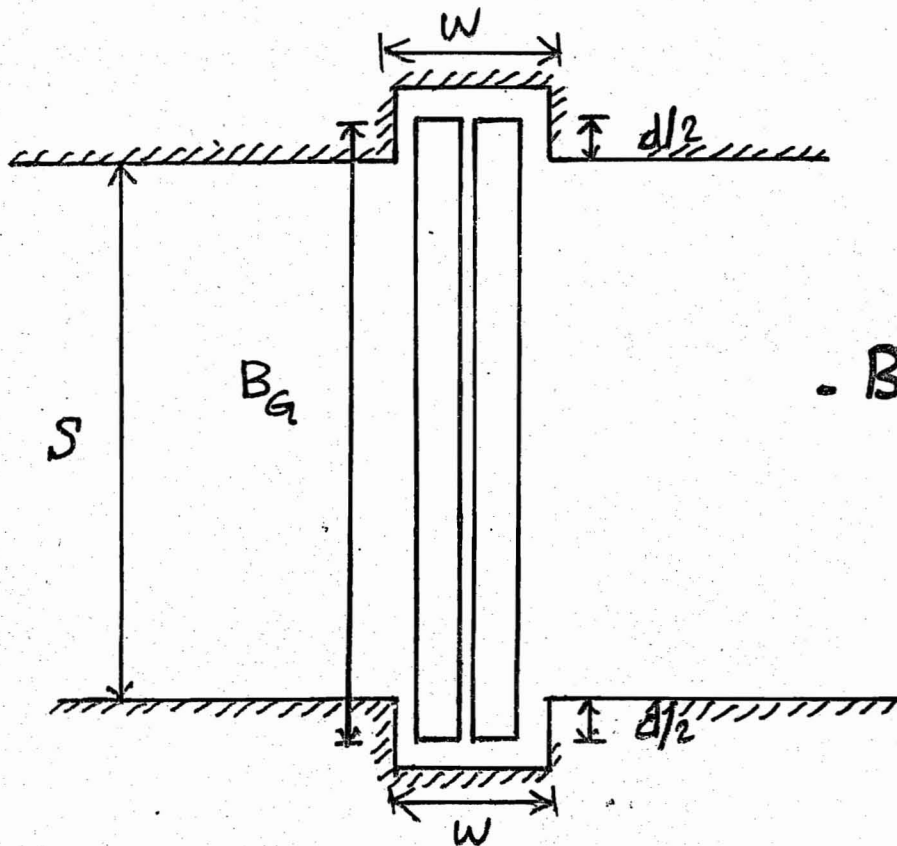
S	3	4	5	6	8
w	0.6	0.75	0.9	1	1.2

Dimensions of double gate



$$H_G = y_{u.s} + (0.3 \rightarrow 0.5)$$

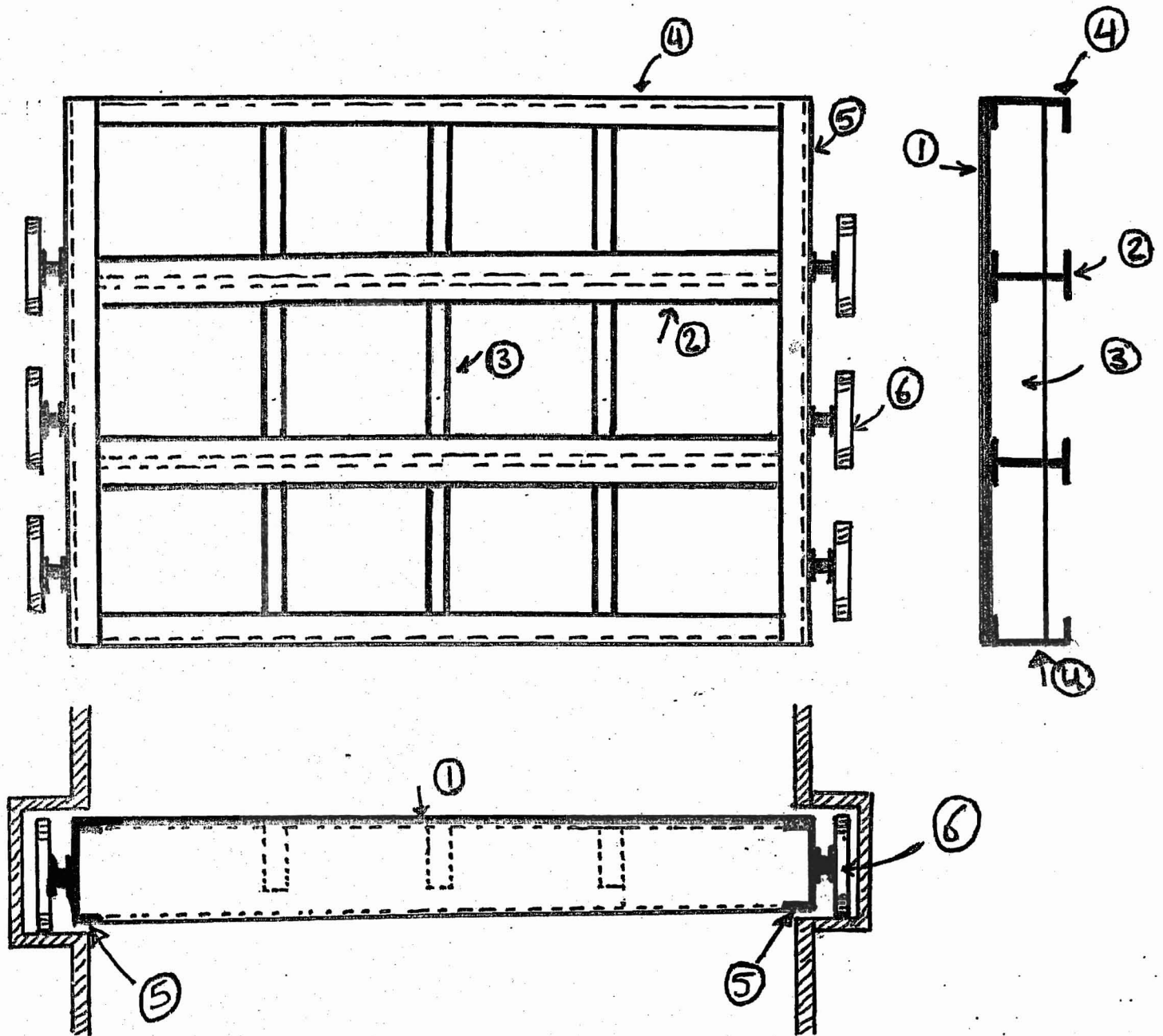
$$H_{1G} = \frac{H_G}{2} + 0.1$$



$$B_G = S + d$$

$$d = \frac{w}{3}$$

Gate Components :-



- 1- Skin Plate
- 2- Horizontal main girder
- 3- Vertical cross girder
- 4- upper and lower beams (C)
- 5- Side beams (C)
- 6- Rollers

Location of main girder

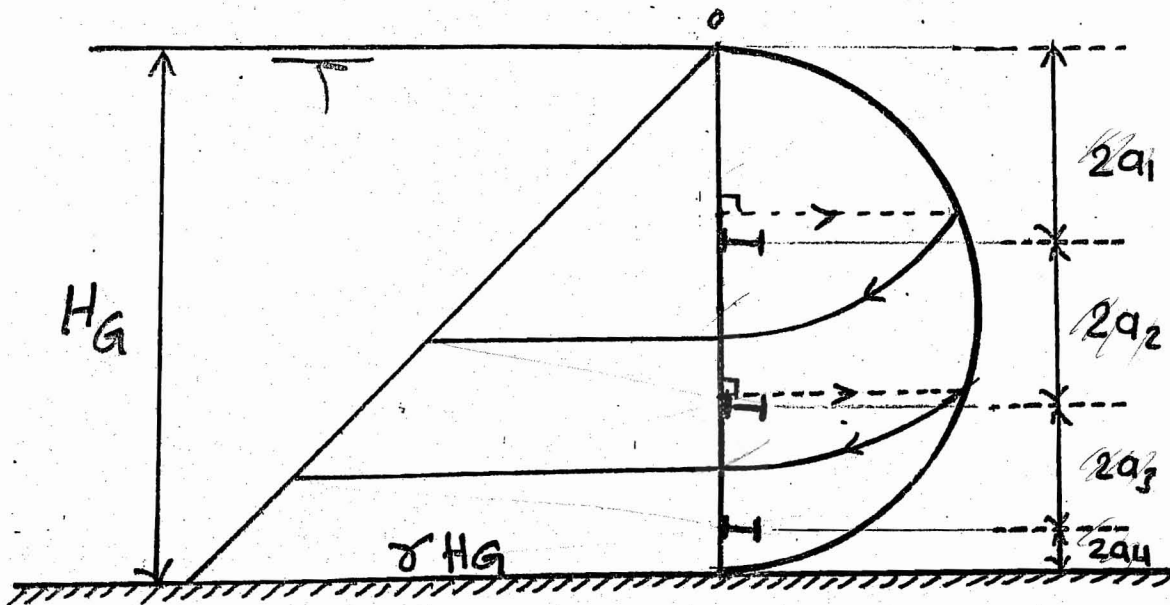
- يتم وضع (main girder) حيث كلاً من γ و δ أقل
- يوجد طريقتان لتحديد مكانه (main girder)

□ - طريقة بيانية

□ - طريقة حسابية

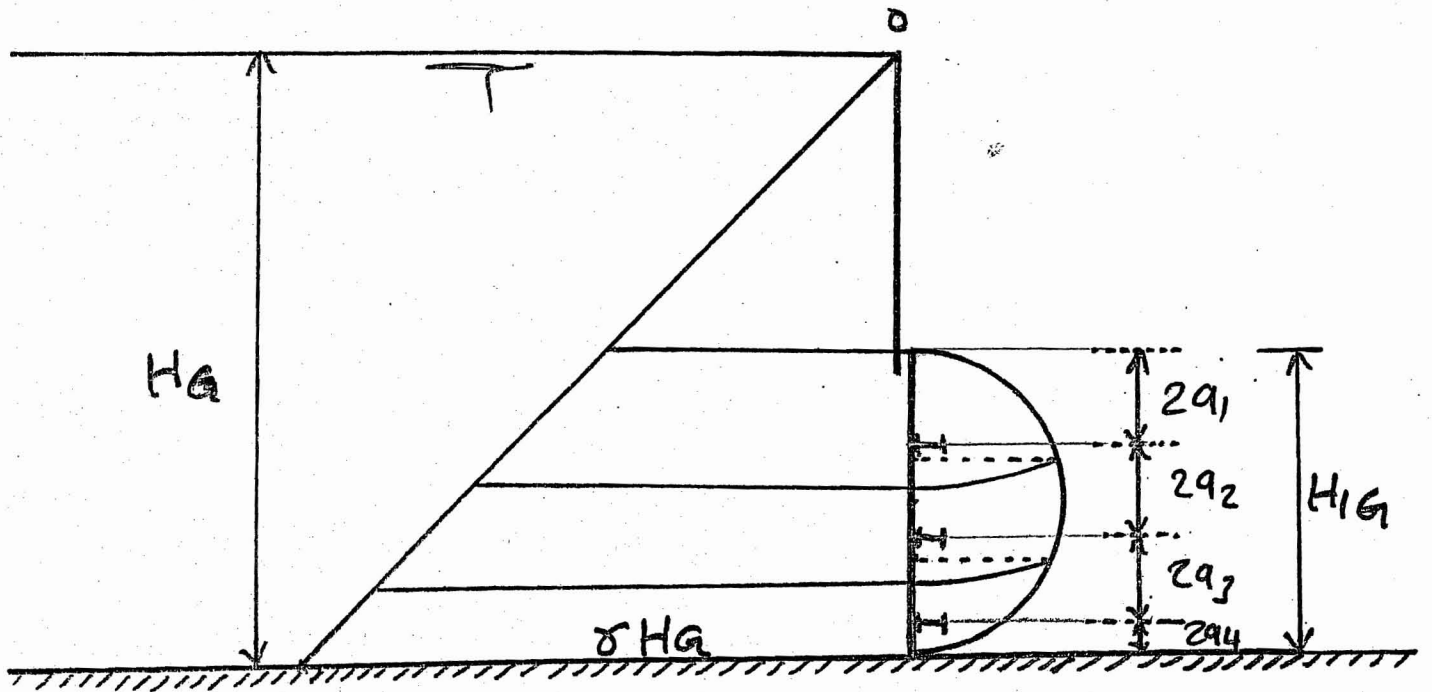
1- Graphical Solution

I. For single gate



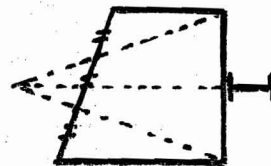
II - for Double Gate :-

يتم تصميم البوابه السفليه وتجهيز التصميم على البوابه العلويه



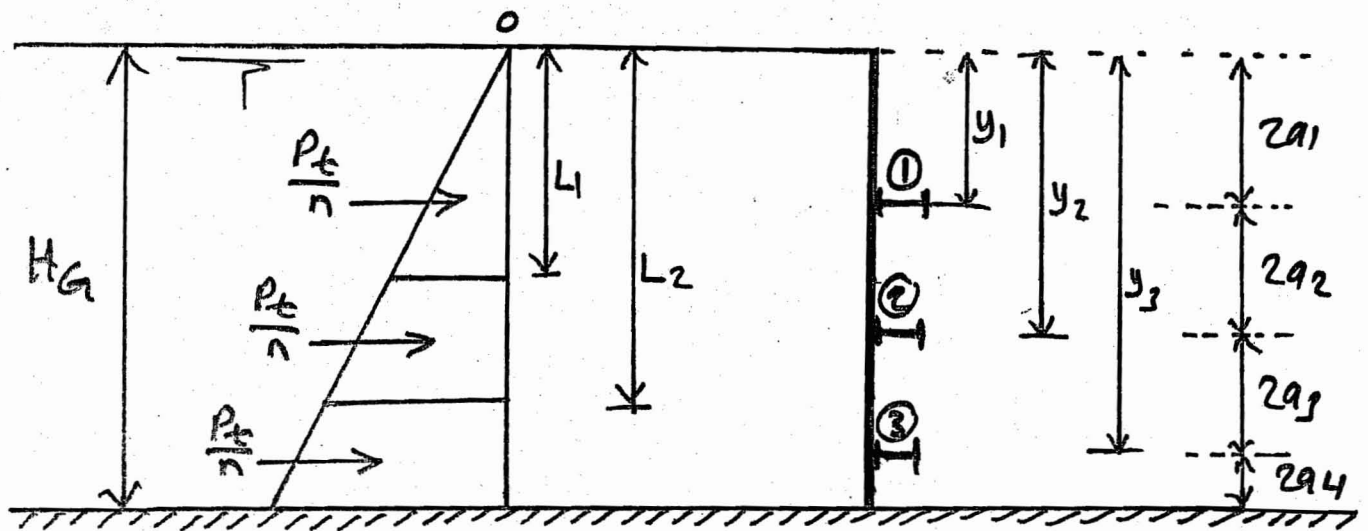
- اذا تم عدد (X.G) أو عدد (M.G) يتم فرضهم كـ α

- يتم وضع (M.G) من مركز الجاه



2- Analytical Solution

I- For single gate :-



$$P_t = \frac{1}{2} \rho \omega H_G^2 B_G = \checkmark$$

for G_1

$$\frac{P_t}{n} = \frac{1}{2} \rho \omega L_1^2 B_G$$

$$\therefore L_1 = \checkmark$$

$$\therefore y_1 = \frac{2L_1}{3}$$

for G_2

$$\frac{P_t}{n} = \frac{1}{2} \sigma_w L_2^2 B_G - \frac{1}{2} \sigma_w L_1^2 B_G$$

$$\therefore L_2 = L$$

$\Sigma M @ 0$

$$\frac{P_t}{n} * y_2 = \frac{1}{2} \sigma_w L_2^2 B_G * \left(\frac{2}{3} L_2\right) - \frac{1}{2} \sigma_w L_1^2 B_G \left(\frac{2}{3} L_1\right)$$

$$\therefore y_2 = L$$

for G_3

$\Sigma M @ 0$

$$\frac{P_t}{n} * y_3 = \frac{1}{2} \sigma_w H_G^2 B_G * \left(\frac{2}{3} H_G\right) - \frac{1}{2} \sigma_w L_2^2 B_G \left(\frac{2}{3} L_2\right)$$

$$\therefore y_3 = L$$

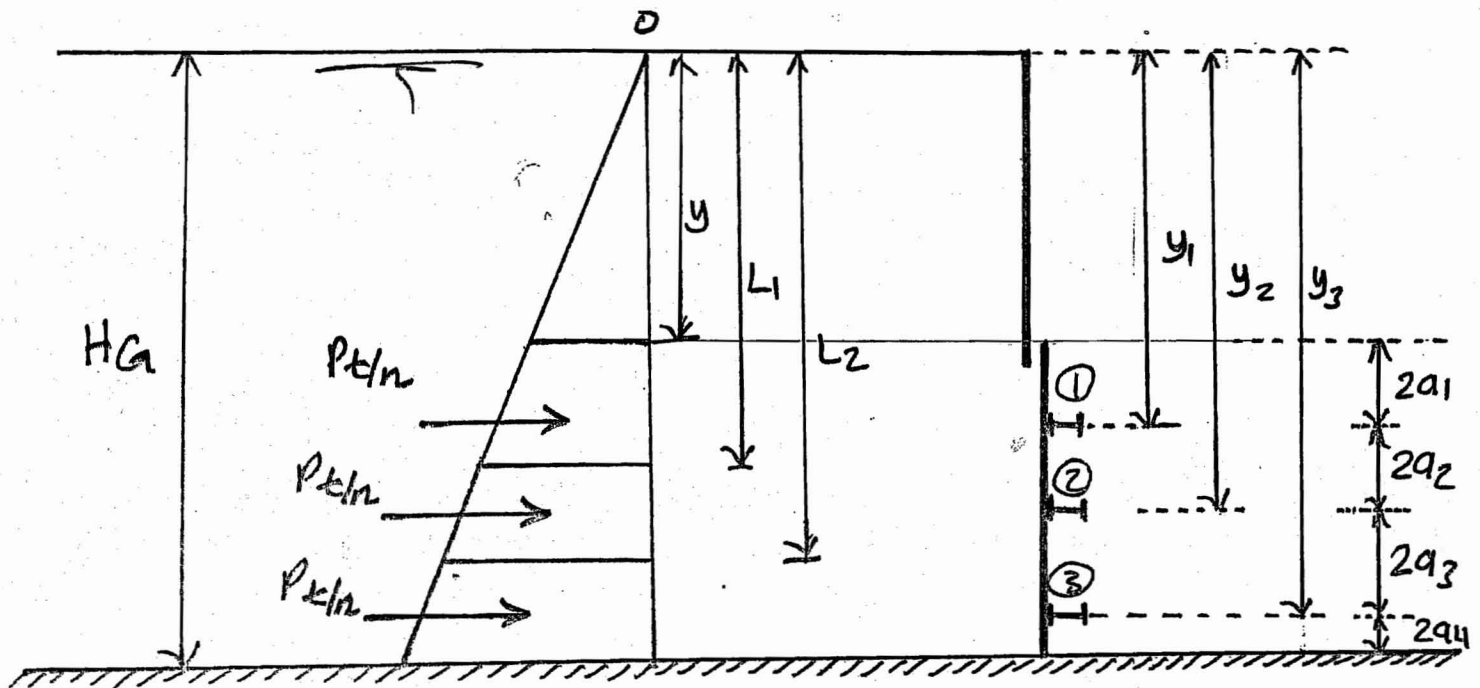
$$\therefore z_{q1} = y_1$$

$$\therefore z_{q2} = y_2 - y_1$$

$$\therefore z_{q3} = y_3 - y_2$$

$$\therefore z_{q4} = H_G - y_3$$

II - For double gate :-



$$P_t = \left(\frac{\gamma_w y + \gamma_w H_G}{2} \right) * H_G * B_G$$

For G_1

$$\frac{P_t}{n} = \frac{1}{2} \gamma_w L^2 B_G - \frac{1}{2} \gamma_w y^2 B_G$$

$$\therefore L_1 = L$$

$\Sigma M @ 0$

$$\frac{P_t}{n} * y_1 = \frac{1}{2} \gamma_w L^2 B_G * \left(\frac{2}{3} L \right) - \frac{1}{2} \gamma_w y^2 B_G * \left(\frac{2}{3} y \right)$$

$$\therefore y_1 = L$$

for G_2

$$\frac{P_t}{n} = \frac{1}{2} \sigma_w L_2^2 B_G - \frac{1}{2} \sigma_w L_1^2 B_G$$

$$\therefore L_2 = L$$

$\Sigma M @ O$

$$\frac{P_t}{n} * y_2 = \frac{1}{2} \sigma_w L_2^2 B_G \left(\frac{2}{3} L_2 \right) - \frac{1}{2} \sigma_w L_1^2 B_G \left(\frac{2}{3} L_1 \right)$$

$$\therefore y_2 = L$$

for G_3

$\Sigma M @ O$

$$\frac{P_t}{n} * y_3 = \frac{1}{2} \sigma_w H_G^2 B_G \left(\frac{2}{3} H_G \right) - \frac{1}{2} \sigma_w L_2^2 B_G \left(\frac{2}{3} L_2 \right)$$

$$\therefore y_3 = L$$

$$\therefore z a_1 = y_1 - y$$

$$\therefore z a_2 = y_2 - y_1$$

$$\therefore z a_3 = y_3 - y_2$$

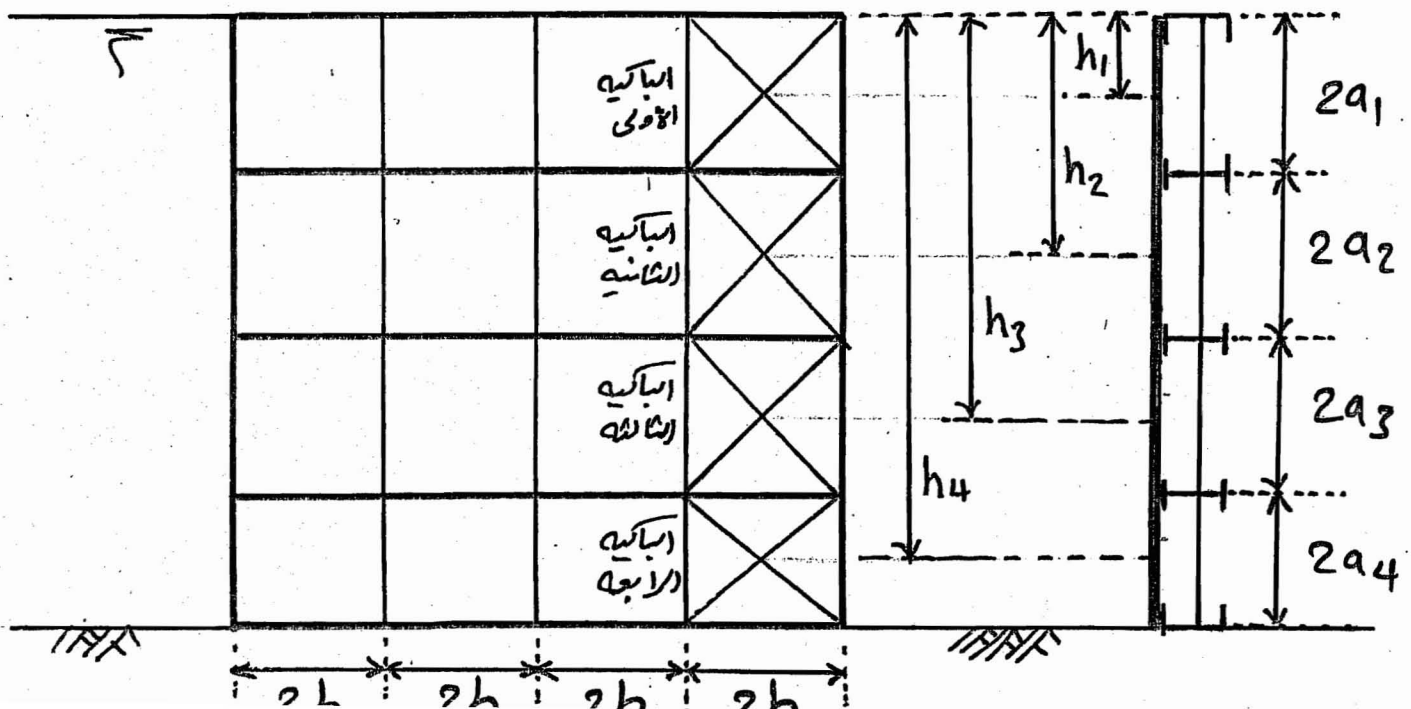
$$\therefore z a_4 = H_G - y_3$$

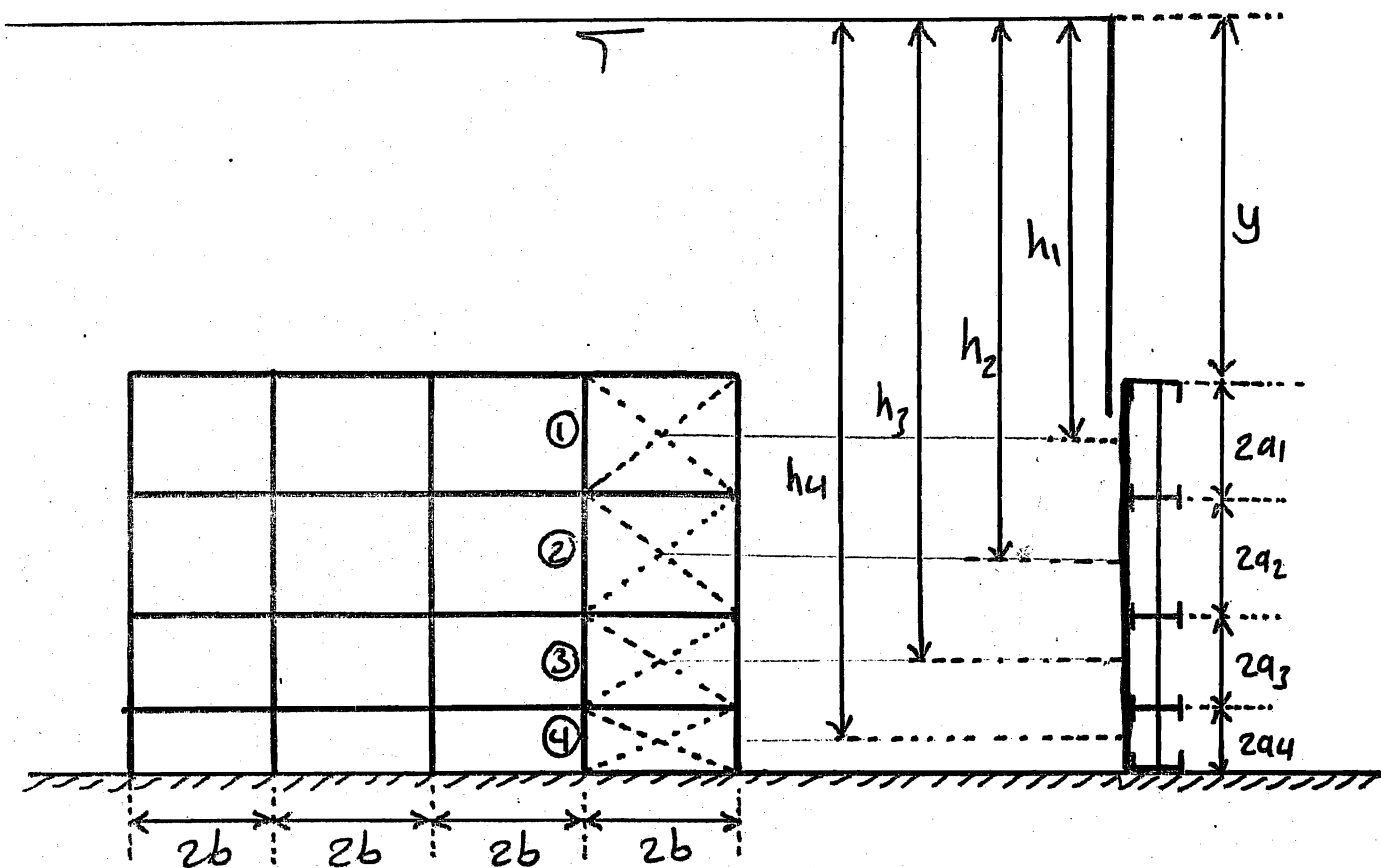
Design of Gate Components

1- Design of Skin Plate :-

$$t = a \cdot b \sqrt{\frac{2 \mu P}{f(a^2 + b^2)}}$$

- . t : Plate thickness (cm)
- . μ : Degree of fixation = 0.94
- . f : Working steel stress = 1 t/cm^2
- . P : ضغط الماء من منتصف بابيه = $\gamma h \text{ (t/m}^2\text{)}$
- . a : نصف عرض (بابيه) = $\frac{2a}{2} \text{ (m)}$
- . b : نصف عرض (بابيه) = $\frac{2b}{2} \text{ (m)}$





- $h_1 = y + \frac{2a_1}{2}$

- $h_2 = y + 2a_1 + \frac{2a_2}{2}$

- $h_3 = y + 2a_1 + 2a_2 + \frac{2a_3}{2}$

- $h_4 = y + 2a_1 + 2a_2 + 2a_3 + \frac{2a_4}{2}$

no.	$a_{(m)}$	$b_{(m)}$	h_m	$P_{(t/m^2)}$	$t_{(cm)}$
1	a_1	b	h_1	δh_1	\checkmark
2	a_2	b	h_2	δh_2	\checkmark
3	a_3	b	h_3	δh_3	\checkmark
4	a_4	b	h_4	δh_4	\checkmark

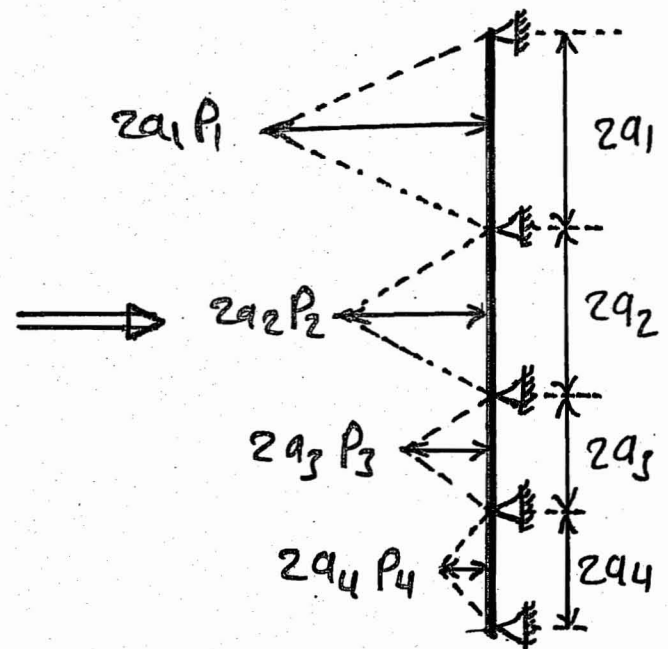
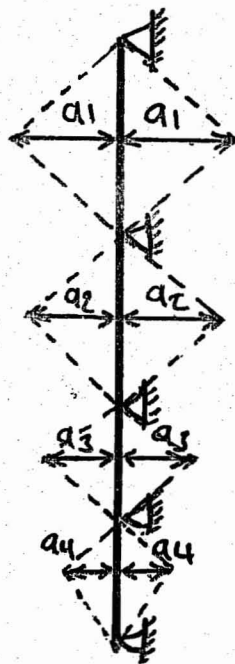
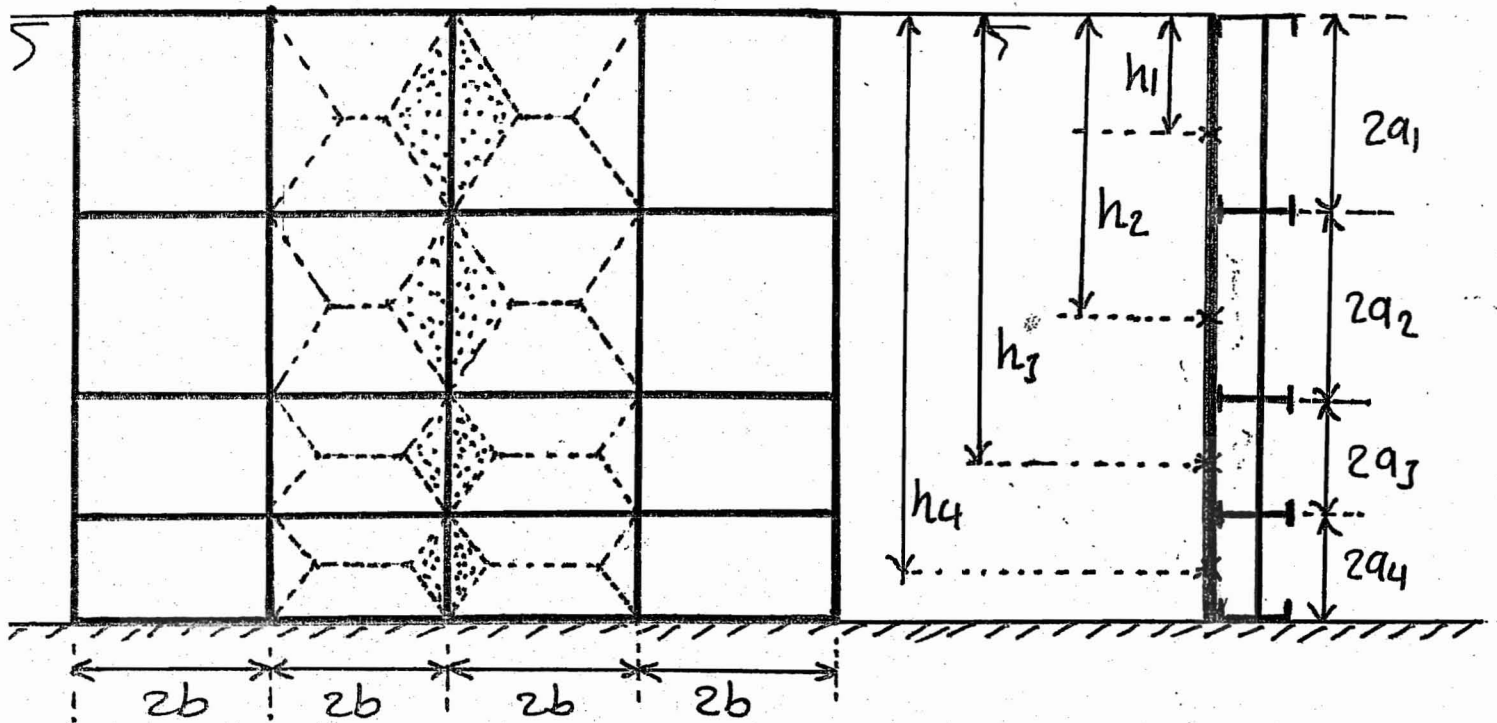
متى اختيار أكبر (t) من الجدول

$$t_{max} = 1 \text{ cm} < 1 \text{ cm}$$

نقرب (t) لأقرب 2 mm و 5 mm

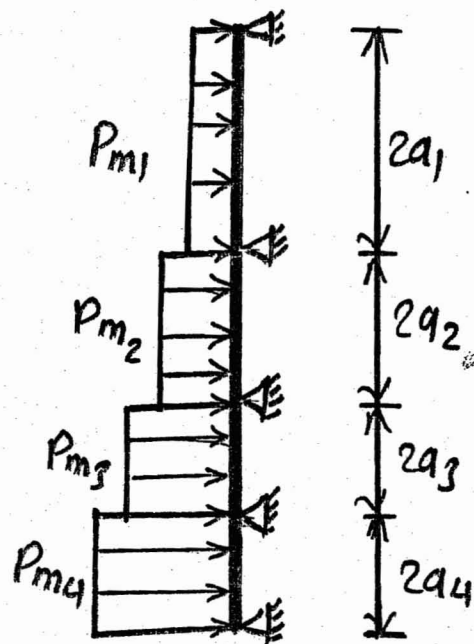
(1, 1.2, 1.4, 1.5, 1.6, 1.8, 2, 2.2, 2.4, 2.5)

2- Design of Cross girder :-



للتحويل من حمل مثالي إلى حمل *uniform* نضرب $\frac{2}{3}$

$$\therefore P_m = \frac{2}{3} (2a p)$$



$$\bullet \quad P_{m1} = \frac{2}{3} (2a_1 p_1)$$

$$\bullet \quad P_{m2} = \frac{2}{3} (2a_2 p_2)$$

$$\bullet \quad P_{m3} = \frac{2}{3} (2a_3 p_3)$$

$$\bullet \quad P_{m4} = \frac{2}{3} (2a_4 p_4)$$

No.	Span (m)	$P = \gamma h$ (t/m ²)	P_m (t/m)	M (t.m)
1	$2a_1$	$P_1 = \gamma h_1$	P_{m1}	$\frac{P_{m1}(2a_1)^2}{8}$
2	$2a_2$	$P_2 = \gamma h_2$	P_{m2}	$\frac{P_{m2}(2a_2)^2}{8}$
3	$2a_3$	$P_3 = \gamma h_3$	P_{m3}	←
4	$2a_4$	$P_4 = \gamma h_4$	P_{m4}	←

M_{max} سے پہلے کا

$$\therefore z = \frac{M_{max}^{t.m}}{f} = \frac{M_{max} \times 10^5}{1000} = \text{cm}^3$$

$f = 1000 \text{ kg/cm}^2$

Choose from table SIB No -----

Sheet (3) Regulators

1- Figure (1) shows the D.S cross section of a main canal in which a reinforced concrete regulator is to be constructed. The regulator consists of 4 vents each 3.0 m width. The maximum discharge through the regulator is $Q = 50 \text{ m}^3/\text{sec}$ and the maximum heading up is 10 cm. The following data are also considered in the design: (i) The bridge width = 10.0 m and it has 2 sidewalks of 1.0 m each, (ii) The pier width = 1.0 m, (iii) Box and sloping wing walls are used for upstream and downstream sides, respectively, and (iv) Vertical sliding steel gates with four Main girders are used

It is required to:

- Check the value of heading up for fully open gates.
- Give a complete structure design of the gate, and find the required lifting force.
- Draw neat sketch showing each of the following views:
 - Plan (H.E.R.)
 - Longitudinal section through a vent centerline.

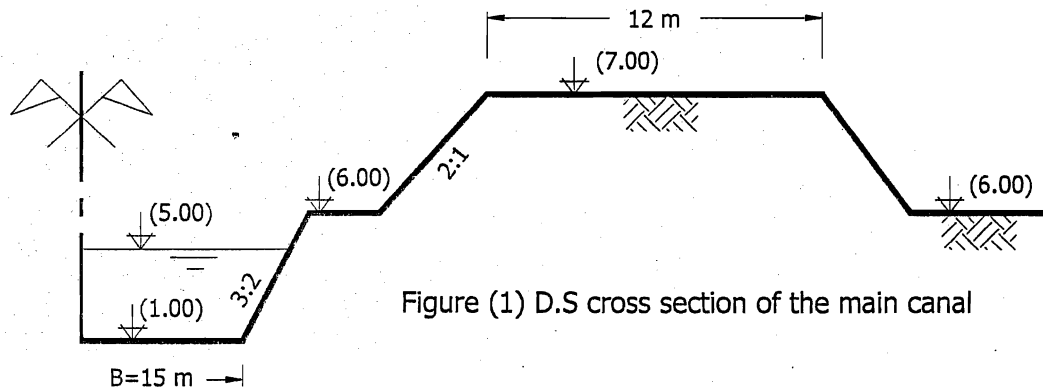


Figure (1) D.S cross section of the main canal

2- A reinforced concrete head regulator with 200.0 m approach channel is to be constructed to feed a main canal from a Rayah. The cross sections data for the canal and Rayah at the crossing site are given in the following table. The available data for the regulator are:

- Maximum allowable discharge through the canal is $6.8 \times 10^6 \text{ m}^3/\text{day}$
- The span of vents is 5.0 m,
- The bridge width over the regulator is 10.0 m and it has two sidewalks of 1.0 m width for each,
- U.S and D.S box wing walls are used,
- The width of the intermediate piers is 1.0 m.

Prob(1)

b-

• $S = 3.0^m$

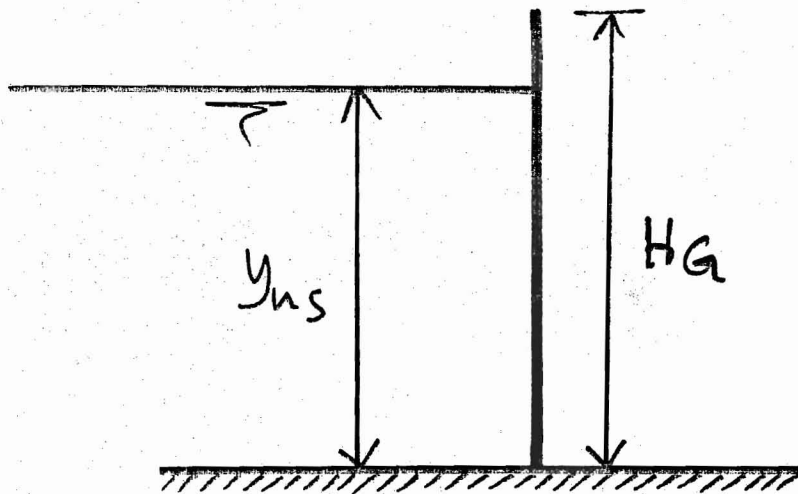
• $y_{ds} = 4.0^m$

$S * y_{ds} = 3 * 4 = 12 \text{ m}^2 < 16 \text{ m}^2$

So use single gate

• $y_{us} = y_{ds} + h_{wp} = 4 + 0.057 = 4.057^m$

• $\therefore S' = 3^m \xrightarrow{\therefore} w = 0.6^m \xrightarrow{\therefore} d = \frac{w}{3} = 0.2^m$



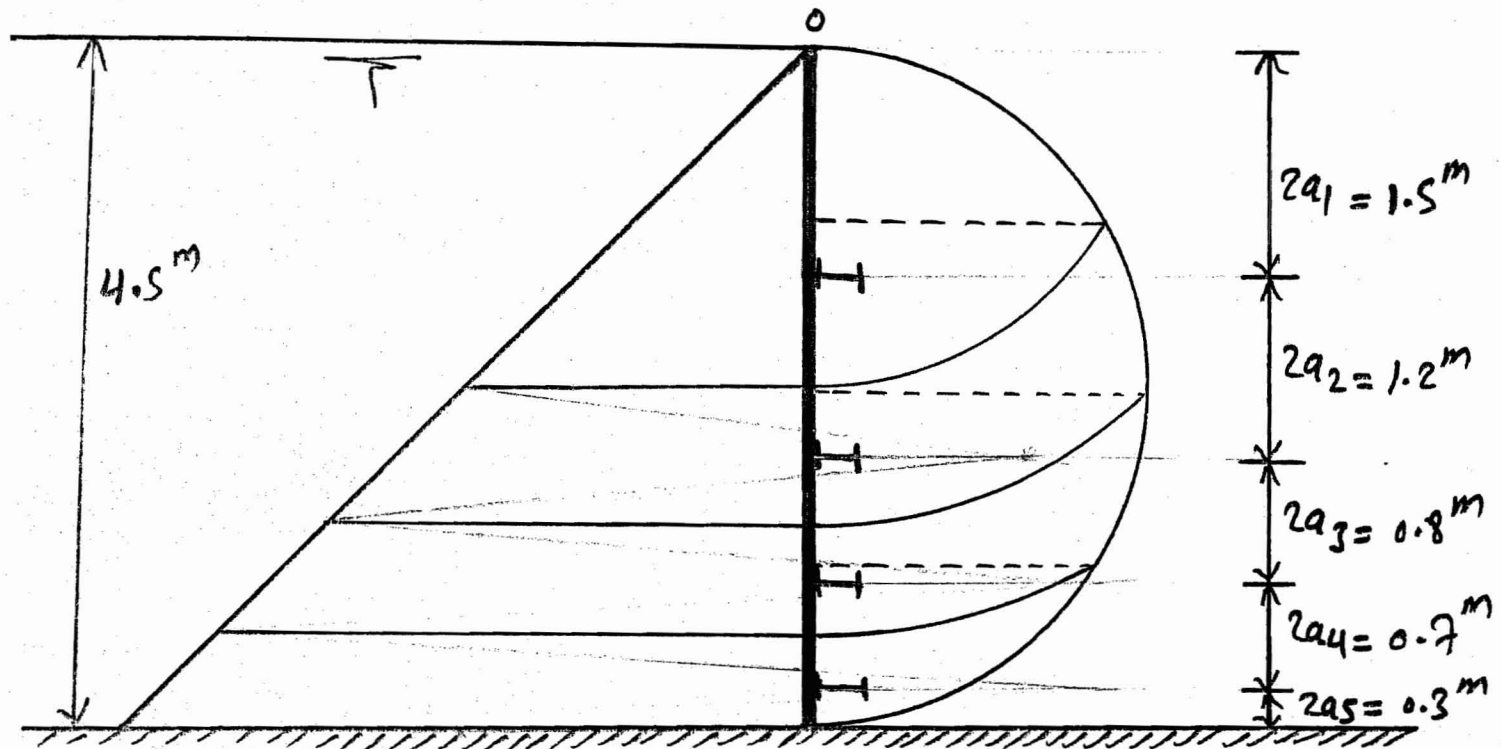
• $H_G = y_{us} + (0.3 \rightarrow 0.5^m) = 4.357 \rightarrow 4.557$

take $H_G = 4.5^m$

• $B_G = S' + d = 3 + 0.2 = 3.2^m$

* Location of main girders

Scale 1:50



* Design of Skin Plate

take No. of X.G = 3.0 $\rightarrow \therefore 2b = \frac{B.G}{4} = 0.8\text{m}$

No	$a_{(m)}$	$b_{(m)}$	$h_{(m)}$	$P_{(t/m^2)}$	$t_{(cm)}$
1	0.75	0.4	0.75	0.75	0.42
2	0.6	0.4	2.1	2.1	0.66
3	0.4	0.4	3.4	3.4	0.72
4	0.35	0.4	3.85	3.85	0.71
5	0.15	0.4	4.35	4.35	0.4

$\therefore t_{max} = 0.72\text{cm}$

So take

$t = 1.0\text{cm}$

* Design of cross girder

No.	Span (m)	$P = \gamma h$ (t/m ²)	P_m (t/m)	M (t.m)
1	1.5	0.75	0.75	0.21
2	1.2	2.1	1.68	0.3
3	0.8	3.4	1.81	0.14
4	0.7	3.85	1.8	0.11
5	0.3	4.35	0.87	0.0098

$$\therefore M_{\max} = 0.3 \text{ t.m}$$

$$\therefore Z = \frac{0.3 \times 10^5}{1000} = 30 \text{ cm}^3$$

Choose from table SIB No.